

Sequential Experimental Designs for Kriging Model

Yongdao Zhou

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Outline

- 1 Introduction
- 2 Pointwise sequential criteria
- 3 Batch sequential design
- 4 Simulations
- 5 Concluding remarks

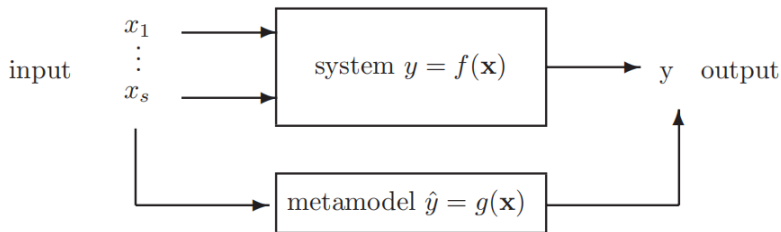
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Introduction

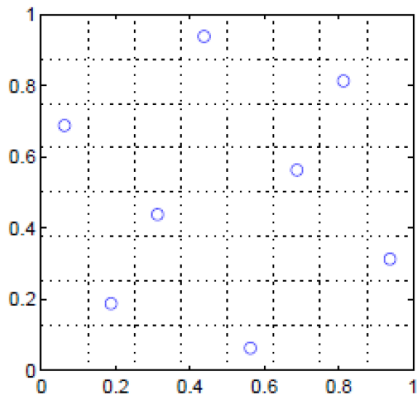
Computer experiments have been widely used in industry, aerospace and other fields due to their high efficiency.

- Computer experiments: samples with the same input setting will produce identical outputs.
- Scientists and engineers make use of computer simulations to explore the complex relationship between inputs and outputs.

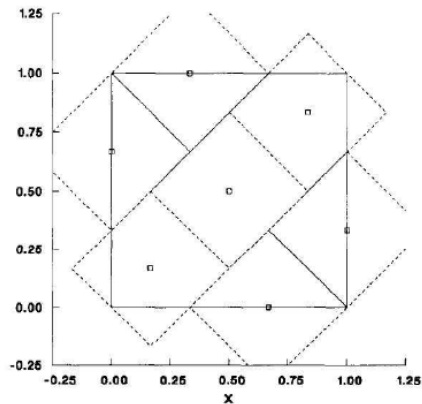


- One of the goals of computer experiments is to find an approximate model that is much simpler than the true (but complicated) model by simulating the behavior on a computer.
- The good properties of **Kriging model**:
 - **Exact interpolation**: Perfectly fits all observed points.
 - **Uncertainty quantification**: Provides not only a prediction but also a predictive variance at any unobserved point.
- Use space-filling design to gather the most information, so that the model can ultimately achieve the goal of **global fitting**.
 - Latin hypercube design
 - Maximin distance design
 - Uniform design

Space-filling design

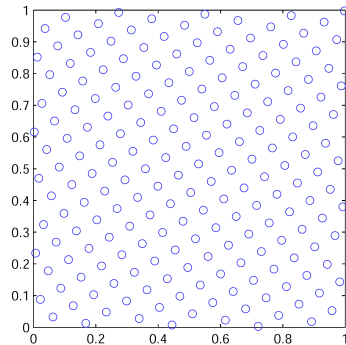
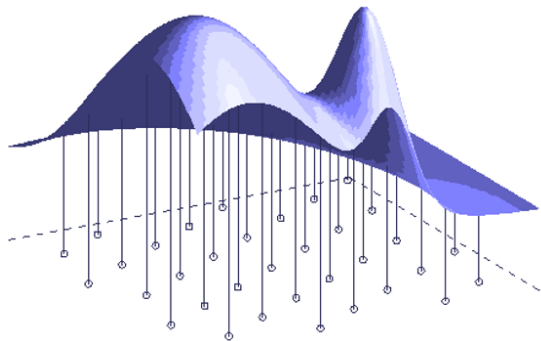


Latin hypercube design



maximin distance design

Uniform design



Theory of uniform design:

- **Uniformity criteria** (Fang and Wang (1994), Zhou and Xu (2014, JASA))
- **Construction methods** (Zhou and Xu (2015, Biometrika), Zhou and Xu (2017, JASA), Fang, Liu, Qin and Zhou (2018, [Springer](#)))

Kriging model

Kriging model is a Gaussian process regression:

$$y(\mathbf{x}) = f(\mathbf{x})^T \beta + z(\mathbf{x}),$$

where $z(\mathbf{x})$ is the zero-mean stationary Gaussian process with the covariance structure

$$\text{Cov}(Z(\mathbf{x}), Z(\mathbf{y})) = \tau^2 k(\mathbf{x}, \mathbf{y}),$$

and τ^2 represents the variance.

- Gaussian separable kernel:

$$k(\mathbf{x}, \mathbf{y}; \theta) = \exp \left\{ - \sum_{t=1}^m \theta_t |x_t - y_t|^2 \right\} + g \delta(\mathbf{x}, \mathbf{y}).$$

- Matérn correlation function:

$$k(\mathbf{x}, \mathbf{y}; \nu, \ell) = \frac{1}{\Gamma(\nu) 2^{\nu-1}} (2\sqrt{\nu} \ell \|\mathbf{x} - \mathbf{y}\|)^{\nu} K_{\nu}(2\sqrt{\nu} \ell \|\mathbf{x} - \mathbf{y}\|).$$

Kriging model

According to the observation points $\mathbf{X} = (\mathbf{x}_1, \dots, \mathbf{x}_n)^T$ and their observation values $\mathbf{Y}_\mathbf{X} = (Z(\mathbf{x}_1), \dots, Z(\mathbf{x}_n))$, we can compute the prediction and its variance at an unobserved point $\mathbf{x}$.

- Prediction: $\hat{y}_\mathbf{X}(\mathbf{x}) = \mathbf{r}_\mathbf{X}^T(\mathbf{x})\mathbf{K}^{-1}(\mathbf{X})\mathbf{Y}_\mathbf{X}$;
- Variance: $\hat{s}_\mathbf{X}^2(\mathbf{x}) = \tau^2 (k(\mathbf{x}, \mathbf{x}) - \mathbf{r}_\mathbf{X}^T(\mathbf{x})\mathbf{K}^{-1}(\mathbf{X})\mathbf{r}_\mathbf{X}(\mathbf{x}))$.

where $\mathbf{r}_\mathbf{X}(\mathbf{x}) = (k(\mathbf{x}, \mathbf{x}_1), \dots, k(\mathbf{x}, \mathbf{x}_n))^T$ and $\mathbf{K}(\mathbf{X}) = (k(\mathbf{x}_i, \mathbf{x}_j))_{n \times n}$.

However, single-stage experiments (i.e., all experimental points are predetermined in a single step) have the following limitations.

- Relies entirely on a priori assumptions about the experimental domain and the true model.
- Cannot dynamically adjust observation points based on existing information.
- May lead to poor model fitting if key regions are omitted.

Therefore, a **sequential experimental design** strategy is necessary.

Algorithm 1 Sequential design for Kriging model

- 1: Select a space-filling design as the initial design $\mathbf{X}_0$.
 - 2: $i \leftarrow 0$.
 - 3: **while** termination condition is not satisfied **do**
 - 4: $\mathbf{Y}_{\mathbf{X}_i} \leftarrow$ the observed values of $\mathbf{X}_i$.
 - 5: Select $\mathbf{B}_{i+1}$ according to the criterion ϕ .
 - 6: $\mathbf{X}_{i+1} \leftarrow (\mathbf{X}_i, \mathbf{B}_{i+1})$.
 - 7: $i \leftarrow i + 1$.
 - 8: **end while**
 - 9: Fit the Kriging model using the final $\mathbf{X}_i$ and $\mathbf{Y}_{\mathbf{X}_i}$.
-

Existing sequential design criteria

For a given criterion ϕ , the next point $\tilde{\mathbf{x}}$ to be added is the point that maximizes $\phi(\mathbf{x})$ in the experimental region $\mathcal{X}$, that is,

$$\tilde{\mathbf{x}} = \arg \max_{\mathbf{x} \in \mathcal{X}} \phi(\mathbf{x}).$$

- ϕ_{MD} is the negative of mixture discrepancy (MD)¹;
- $\phi_s(\mathbf{x}) = \hat{s}_{\mathbf{X}}^2(\mathbf{x})$;
- $\phi_{El_0}(\mathbf{x}) = (\hat{y}_{\mathbf{X}}(\mathbf{x}) - f(\mathbf{x}^*))^2 + \hat{s}_{\mathbf{X}}^2(\mathbf{x})$;
- $\phi_{El_1}(\mathbf{x}) = (\hat{y}_{\mathbf{X}}(\mathbf{x}) - f(\mathbf{x}^*) - \nabla^T f(\mathbf{x}^*)(\mathbf{x} - \mathbf{x}^*))^2 + \hat{s}_{\mathbf{X}}^2(\mathbf{x})$;
- $\phi_{El_2}(\mathbf{x}) = (\hat{y}_{\mathbf{X}}(\mathbf{x}) - f(\mathbf{x}^*) - \nabla^T f(\mathbf{x}^*)(\mathbf{x} - \mathbf{x}^*))^2 \times d(\mathbf{x}, \mathbf{x}^*) + \hat{s}_{\mathbf{X}}^2(\mathbf{x})$.

¹Zhou, Fang and Ning (2013, J Complexity)

Existing sequential designs are mainly divided into two categories.

- Pointwise sequential design: observe **one point** at a time.
 - Advantages: more sufficient information utilization and less likely to fall into local optima.
 - Disadvantages: more iterations and higher resource consumption.
 - **limitations** of current researches: most existing methods lack theoretical guarantees.
- Batch sequential design: observe **multiple points** at a time.
 - Advantages: significantly reduces the number of experimental runs and improves resource utilization efficiency.
 - Disadvantages: prone to falling into local optima.
 - **limitations** of current researches:
 - Observation-based methods are relatively scarce.
 - There is no framework that bridges pointwise sequential design and batch sequential design.

Then, we consider the following improvement.

- Two novel pointwise sequential criteria are proposed, along with corresponding theoretical results.
- A general batch sequential design framework is presented, which can extend any pointwise sequential criterion to batch scenarios.
- The effectiveness and robustness of the proposed methods are verified through simulations on multiple test functions.

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Gradient-based criterion: motivation

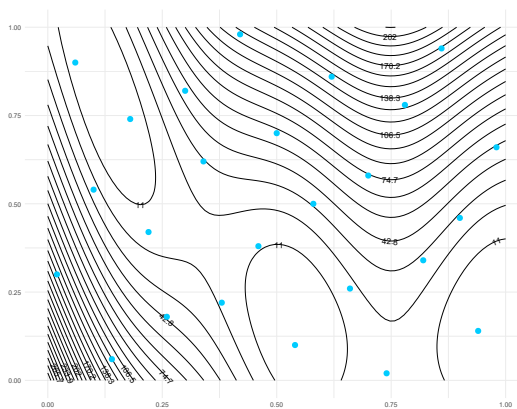
- Consider the Branin function as an example:

$$f(x_1, x_2) = \left(15x_2 - \frac{5.1}{4\pi^2}(15x_1 - 5)^2 + \frac{5}{\pi}(15x_1 - 5) - 6 \right)^2 + 10 \left(1 - \frac{1}{8\pi} \right) \cos(15x_1 - 5) + 10.$$

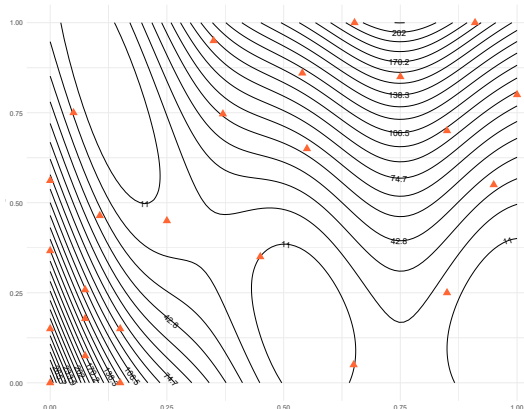
- The kernel function is the Gaussian separable kernel.
- Two methods: uniform design based on mixture discrepancy and gradient-based sequential design.
- Evaluation metrics: root mean square error (RMSE).

$$\text{RMSE}(\mathbf{X}) = \sqrt{\frac{\sum_{\mathbf{x} \in \mathbf{X}_{\text{test}}} (f(\mathbf{x}) - \hat{y}(\mathbf{x}))^2}{n}}.$$

Gradient-based criterion: motivation



(a) Uniform design



(b) Gradient-based sequential design.

Gradient-based sequential design is dense in regions with large gradients and sparse in regions with small gradients, and maintain overall uniformity across the entire design space

Gradient-based criterion: motivation

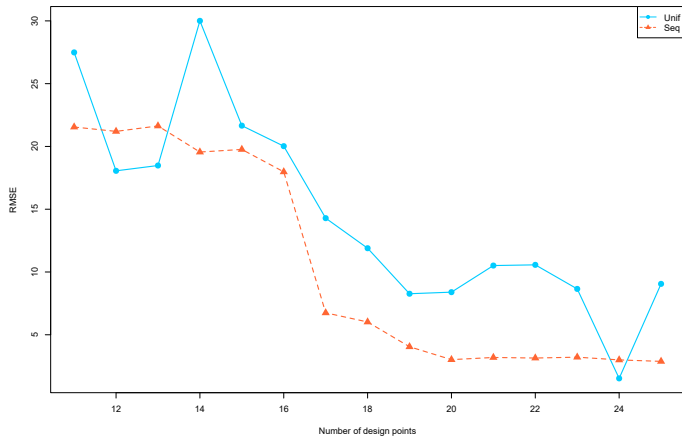


Figure: The RMSE of the uniform design and the gradient-based sequential design with different number of design points.

Gradient-based criterion: theoretical results

The following theorem shows that the upper bound of the pointwise error is controlled by ϕ_{gra} .

Theorem

Let $f(\mathbf{x})$ be the smooth true model and $\hat{y}_{\mathbf{X}}(\mathbf{x})$ be the predicted value of the Kriging model at point $\mathbf{x}$ based on $\mathbf{X}$. Then for any $\mathbf{x} \in \mathcal{X}$, we have

$$|f(\mathbf{x}) - \hat{y}_{\mathbf{X}}(\mathbf{x})| \leq \|\nabla f(\mathbf{t})\| \times d(\mathbf{x}, \mathbf{x}^*) + |\hat{y}_{\mathbf{X}}(\mathbf{x}) - f(\mathbf{x}^*)|,$$

where $\mathbf{x}^* = \arg \min_{\mathbf{y} \in \mathbf{X}} d(\mathbf{x}, \mathbf{y})$ and $\mathbf{t} \in \{\alpha \mathbf{x} + (1 - \alpha) \mathbf{x}^* \mid 0 \leq \alpha \leq 1\}$.

Gradient-based criterion: expression

Gradient-based criterion:

$$\phi_{gra}(\mathbf{x}) = \sqrt{E(\|\nabla f(\mathbf{x})\|^2)} \times d(\mathbf{x}, \mathbf{x}^*) + |\hat{y}_{\mathbf{x}}(\mathbf{x}) - f(\mathbf{x}^*)|,$$

where $\mathbf{x}^*$ is the point in the existing design that is closest to $\mathbf{x}$.

- $\sqrt{E(\|\nabla f(\mathbf{x})\|^2)}$: add points where gradient is large.
- $d(\mathbf{x}, \mathbf{x}^*)$: keep all points uniformly distributed.
- $|\hat{y}_{\mathbf{x}}(\mathbf{x}) - f(\mathbf{x}^*)|$: add points where variation is large.

Variance-based criterion: motivation

- Sacks and Schiller (1988) proposed a criterion that selects the point minimizing the maximum prediction variance $\hat{s}_{\mathbf{x}}^2(\mathbf{x})$.
- Relying solely on the prediction variance of design point estimates is insufficient to fully characterize the overall estimation error.
- The estimation error is also governed by the variance of the gradient estimate.

Variance-based criterion: theoretical results

Theorem

Let $\mathcal{X} \subseteq \mathbb{R}^m$ be open, $\mathcal{N}_k(\mathcal{X})$ be the native Hilbert space corresponding to the symmetric positive definite kernel $k(\mathbf{x}, \mathbf{y}) \in \mathcal{C}^{2m}(\mathcal{X}, \mathcal{X}) : \mathcal{X} \times \mathcal{X} \rightarrow \mathbb{R}$ and f be the smooth true function. Denote the i -th diagonal element of $\nabla^2 k(\mathbf{x}, \mathbf{x}) - \nabla r_{\mathbf{X}}^T(\mathbf{x}) \mathbf{K}^{-1}(\mathbf{X}) \nabla r_{\mathbf{X}}(\mathbf{x})$ as $g_i(\mathbf{x})$. Then we have

- $|f(\mathbf{x}) - \hat{y}_{\mathbf{X}}(\mathbf{x})| \leq \sqrt{k(\mathbf{x}, \mathbf{x}) - \mathbf{r}_{\mathbf{X}}^T(\mathbf{x}) \mathbf{K}^{-1}(\mathbf{X}) \mathbf{r}_{\mathbf{X}}(\mathbf{x})} \times |f|_{\mathcal{N}_k(\mathcal{X})},$
- $|f(\mathbf{x}) - \hat{y}_{\mathbf{X}}(\mathbf{x})| \leq \sqrt{\sum_{i=1}^m g_i(\mathbf{t})} \times d(\mathbf{x}, \mathbf{x}^*) \times |f|_{\mathcal{N}_k(\mathcal{X})},$

where $\mathbf{t} \in \{\alpha \mathbf{x} + (1 - \alpha) \mathbf{x}^* \mid 0 \leq \alpha \leq 1\}$ and $|f|_{\mathcal{N}_k(\mathcal{X})}$ is the norm of function f in the native space $\mathcal{N}_k(\mathcal{X})$.

Variance-based criterion: expression

Thus, we present the specific expression for the variance-based criterion as

$$\phi_{var}(\mathbf{x}) = \min \left(\sqrt{k(\mathbf{x}, \mathbf{x}) - \mathbf{r}_{\mathbf{X}}^T(\mathbf{x}) \mathbf{K}^{-1}(\mathbf{X}) \mathbf{r}_{\mathbf{X}}(\mathbf{x})}, \sqrt{\sum_{i=1}^m g_i(\mathbf{x}) \times d(\mathbf{x}, \mathbf{x}^*)} \right).$$

When the number of current design points is n and the dimension is m , the computational complexity of both ϕ_{gra} and ϕ_{var} is $O(n^3 + mn^2)$.

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Cluster-based top- b sequential design: motivation

- Simply selecting the b points that maximize $\phi(\mathbf{x})$ would inevitably cluster around the global maximum point, leading to the inherent problem of point clustering.
- In fact, each iteration yields more information beyond the maximum point.
- The current local maximum could become the global maximum in the next iteration.

Idea: Apply clustering to select multiple local maximum points in each iteration.

Cluster-based top- b sequential design: algorithm

Algorithm 2 The selection of B_i in top- b sequential design

```
1: Input:  $D_{all}$ ,  $\phi(\mathbf{x})$ ,  $b$ ,  $\alpha$ ,  $\beta$ 
2: Sort the points in  $D_{all}$  by their  $\phi$  values in descending order and denoted them
   as  $\mathbf{x}_{(1)}, \dots, \mathbf{x}_{(n_{all})}$ 
3:  $Cluster = \{\{\mathbf{x}_{(1)}\}\}$ 
4: for  $i = 2$  to  $n_{all}$  do
5:   if the number of clusters in  $Cluster$  is  $b$  then
6:     break
7:   end if
8:   for each cluster  $C$  in  $Cluster$  do
9:     if the number of points in  $C$  is greater than 1 then
10:       $\bar{d} \leftarrow$  the average distance of each point in  $C$  to the cluster centroid
11:       $d \leftarrow$  the distance between point  $\mathbf{x}$  and the centroid
12:      if  $d < \beta \bar{d}$  then
13:        Assign  $\mathbf{x}_{(i)}$  to cluster  $C$ 
14:        break
15:      end if
16:    end if
17:    if the number of points in  $C$  is 1 then
18:      Denote the point in  $C$  as  $\mathbf{x}_C$ 
19:       $num \leftarrow$  the number of points in the cube formed by  $\mathbf{x}_C$  and  $\mathbf{x}$ 
20:      if  $num \leq \alpha$  then
21:        Assign  $\mathbf{x}_{(i)}$  to cluster  $C$ 
22:        break
23:      end if
24:    end if
25:  end for
26:  Add  $\mathbf{x}_{(i)}$  as a new cluster to  $Cluster$ .
27: end for
28: Output: the first point of each cluster in  $Cluster$ 
```

Cluster-based top- b sequential design: algorithm

- D_{all} : uniform design for discretizing the design space.
- α and β govern the cluster assignment of candidate points.
 - Small value: produces overly small clusters and leads to point clustering.
 - Large value: may result in excessively large clusters that hinder local optimum selection.
 - The sensitivity analysis shows that $\alpha = 10$ and $\beta = 5$ perform favorably.
- For the choice of the parameter b , it generally depends on the practical scenario.
 - Large b : reduces the number of iterations and thus saves computational resources.
 - Small b : allows more precise selection of observation points and improves model accuracy.
 - In general, values of b ranging from 2 to 5 are suitable.

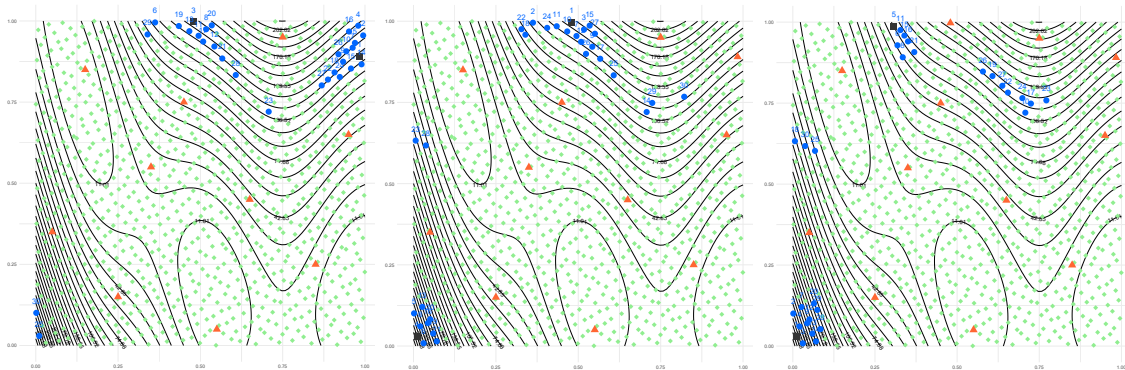
Cluster-based top- b sequential design: example

- The true response model is the Branin function.
- Discretize $\mathcal{X} = [0, 1]^2$ using a uniform design $\mathbf{D}_{all}$ with 1000 points, and select $\mathbf{B}_i$ from $\mathbf{D}_{all}$.

The following three figures show the pointwise sequential designs corresponding to the cases where the numbers of points are 10, 11, and 12, respectively.

- Red triangles: current design $\mathbf{X}_i$.
- Green diamonds: points in $\mathbf{D}_{all}$.
- Blue circles: top 30 points in $\mathbf{D}_{all}$ that maximize $\phi_{gra}(\mathbf{x})$.
- Black squares: the points selected by clustering $\mathbf{D}_{all}$ and choosing the maximum ϕ_{gra} point in the first two clusters (Algorithm 2).

Cluster-based top- b sequential design: example



Cluster-based top- b sequential design: example

- The points maximizing ϕ_{gra} tend to exhibit a clustering pattern.
- The point labeled 3 in the first figure becomes the new maximizer of $\phi_{gra}(\mathbf{x})$ in the second figure, and so on.
- Thus, we can directly select both the point labeled 1 and the point labeled 3 for simultaneous observation in the first iteration.
- This batch design selection strategy not only reduces the cost of additional iterative observations but also yields outcomes that are comparable to those of the pointwise sequential design.

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Test functions

- f_1 : the Branin function.
- $f_2(x_1, x_2) = \left(1 - \exp\left(-\frac{0.5}{x_2}\right)\right) \frac{2300x_1^3 + 1900x_1^2 + 2092x_1 + 60}{100x_1^3 + 500x_1^2 + 4x_1 + 20}$.
- $f_3(x_1, x_2) = \log(2 + \sin(2\pi x_1)) \cos(2\pi x_2^2)$.
- Hartman function of dimension three:
$$f_4(x_1, x_2, x_3) = -\sum_{i=1}^4 c_i \exp\left\{-\sum_{j=1}^3 \alpha_{ij}(x_j - p_{ij})^2\right\}.$$
- Ackley function of dimension five:

$$f_5(\mathbf{x}) = -20 \exp\left(-0.2 \sqrt{\frac{1}{5} \sum_{i=1}^5 x_i^2}\right) - \exp\left(\frac{1}{5} \sum_{i=1}^5 \cos(2\pi x_i)\right) + 20 + e.$$

- Zakharov function: $f_6(\mathbf{x}) = \sum_{i=1}^m x_i^2 + (\sum_{i=1}^m 0.5ix_i)^2 + (\sum_{i=1}^m 0.5ix_i)^4$.
- Rosenbrock function: $f_7(\mathbf{x}) = \sum_{i=1}^{m-1} [100(x_{i+1} - x_i^2)^2 + (x_i - 1)^2]$.

Comparison results: MAE of pointwise sequential designs

We compare our methods with 5 existing criteria on 7 test functions with dimensions ranging from 2 to 8 under maximum absolute error (MAE).

Table 1: The MAE of different pointwise sequential designs.

Test function	m	ϕ_{EI_0}	ϕ_{EI_1}	ϕ_{EI_2}	ϕ_s	ϕ_{MD}	ϕ_{gra}	ϕ_{var}
f_1	2	49.61	9.85	3.07	3.79	21.30	26.02	2.05
f_2	2	2.41	0.99	0.82	1.24	3.26	0.75	0.97
f_3	2	0.84	0.54	0.26	0.25	0.37	0.99	0.21
f_4	3	1.00	1.17	1.27	1.27	0.96	0.80	0.80
f_5	5	14.49	13.94	14.05	14.65	13.91	14.05	13.69
f_6	3	1.90	2.09	1.15	0.35	1.17	2.60	0.28
f_6	5	235.12	298.32	112.92	213.95	426.67	228.48	186.25
f_6	8	14565	14359	10203	25987	25124	9478	11158
f_7	3	6.92	2.95	2.21	1.44	6.86	6.23	1.41
f_7	5	91.53	163.05	153.94	61.67	147.37	104.37	58.59
f_7	8	235.79	248.43	204.63	179.14	278.62	255.74	177.21

Comparison results: RMSE of pointwise sequential designs

Table 2: The RMSE of different pointwise sequential designs.

Test function	m	ϕ_{EI_0}	ϕ_{EI_1}	ϕ_{EI_2}	ϕ_s	ϕ_{MD}	ϕ_{gra}	ϕ_{var}
f_1	2	4.49	0.72	0.72	1.11	1.70	0.52	0.65
f_2	2	0.43	0.26	0.25	0.35	0.30	0.21	0.23
f_3	2	0.11	0.09	0.07	0.07	0.08	0.06	0.06
f_4	3	0.20	0.21	0.23	0.26	0.20	0.17	0.31
f_5	5	0.91	0.81	0.82	0.77	0.81	0.81	0.77
f_6	3	0.18	0.15	0.10	0.08	0.15	0.22	0.06
f_6	5	24.05	25.32	25.06	28.83	24.92	23.11	35.49
f_6	8	1637.46	1611.18	1162.48	2103.61	1349.59	1207.69	1487.18
f_7	3	0.76	0.42	0.30	0.28	0.59	0.24	0.30
f_7	5	16.06	19.92	15.19	13.18	17.71	15.68	13.25
f_7	8	37.11	42.03	35.40	30.97	47.88	29.61	30.34

Comparison results: MAE of batch sequential designs

Table 3: The MAE of different batch sequential designs.

Test function	m	b	ϕ_{EI_0}	ϕ_{EI_1}	ϕ_{EI_2}	ϕ_s	ϕ_{MD}	ϕ_{gra}	ϕ_{var}
f_1	2	2	4.73	5.63	2.56	3.41	11.41	4.92	1.64
f_1	2	3	4.88	1.94	1.28	0.77	4.18	4.49	0.72
f_1	2	5	5.39	0.36	0.30	0.08	2.66	8.00	0.11
f_2	2	2	1.95	1.08	1.03	0.85	4.32	0.90	0.83
f_2	2	3	1.33	0.99	0.42	0.39	1.39	1.66	0.38
f_2	2	5	0.56	0.50	0.32	0.37	0.66	0.69	0.21
f_3	2	2	0.62	0.65	0.30	0.25	1.09	0.68	0.21
f_3	2	3	0.31	0.15	0.23	0.09	0.25	0.41	0.11
f_3	2	5	0.18	0.07	0.10	0.06	0.31	0.12	0.05
f_4	3	2	1.27	1.19	0.84	1.28	1.11	1.21	1.49
f_4	3	3	1.20	1.19	0.87	1.00	0.90	1.18	0.84
f_4	3	5	1.00	0.94	0.87	0.54	0.82	1.18	1.01
f_5	5	2	13.30	12.66	12.75	13.15	12.78	12.71	11.15
f_5	5	3	11.38	12.86	12.78	12.68	12.68	12.13	12.89
f_5	5	5	12.61	12.92	12.68	12.79	12.55	12.11	11.87

Comparison results: RMSE of batch sequential designs

Table 4: The RMSE of different batch sequential designs.

Test function	m	b	ϕ_{EI_0}	ϕ_{EI_1}	ϕ_{EI_2}	ϕ_s	ϕ_{MD}	ϕ_{gra}	ϕ_{var}
f_1	2	2	0.61	1.26	0.50	7.92	1.62	0.40	0.43
f_1	2	3	0.45	0.24	0.18	0.23	0.42	0.14	0.18
f_1	2	5	0.39	0.03	0.03	0.02	0.15	0.07	0.02
f_2	2	2	0.33	0.23	0.25	0.26	0.28	0.23	0.26
f_2	2	3	0.25	0.18	0.14	0.12	0.24	0.33	0.12
f_2	2	5	0.15	0.10	0.06	0.06	0.08	0.05	0.06
f_3	2	2	0.11	0.09	0.08	0.08	0.11	0.06	0.07
f_3	2	3	0.083	0.042	0.028	0.029	0.032	0.070	0.028
f_3	2	5	0.026	0.011	0.009	0.014	0.019	0.029	0.009
f_4	3	2	0.21	0.21	0.26	0.27	0.21	0.20	0.29
f_4	3	3	0.21	0.23	0.14	0.20	0.14	0.12	0.15
f_4	3	5	0.20	0.13	0.16	0.10	0.11	0.10	0.14
f_5	5	2	1.28	0.83	0.81	0.84	0.81	0.82	0.84
f_5	5	3	0.90	0.81	0.81	0.75	0.77	0.73	0.79
f_5	5	5	0.74	0.73	0.75	0.66	0.67	0.63	0.69

Comparison results

- For the pointwise sequential designs, the best-performing design in most cases is one of the two sequential designs proposed.
- The batch design performs comparably in most cases, and it is slightly outperformed by the pointwise design in a few instances.

How to choose the criterion?

- For the objective of minimizing RMSE: gradient-based criterion.
- For the objective of minimizing MAE: variance-based criterion.

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Concluding remarks

- We introduce two novel criteria: gradient-based criterion and variance-based criterion.
- We put forward a framework termed the cluster-based top- b sequential design approach, which is applicable to any pointwise sequential design criterion.
- Through comparisons with existing criteria and methods, we demonstrate that the proposed criteria exhibit excellent performance and validate the robustness of the proposed batch sequential designs.
- Future work will extend this framework to high-dimensional and constrained design spaces.

Thank you for your attention!

Yongdao Zhou

Nankai University, China